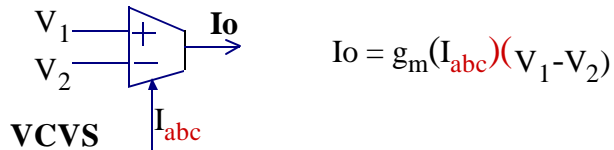


## OPERATIONAL TRANSCONDUCTANCE AMPLIFIER (OTA)

First commercial OTA produced by RCA in 1969, i.e., CA3080



The transconductance gain “ $g_m$ ” is a function of the  $I_{abc}$ .

$$g_m = h_1 I_{abc} \text{ for bipolar and weak inversion MOSFETs}$$

$$g_m = h_2 [I_{abc}]^{1/2} \text{ for MOSFETs in saturation}$$

## Operational Transconductance Amplifier (OTA)

An ideal Op Amp requires high gain

$$A_v = G_m R_{out}$$

High  $R_{out}$  is desirable

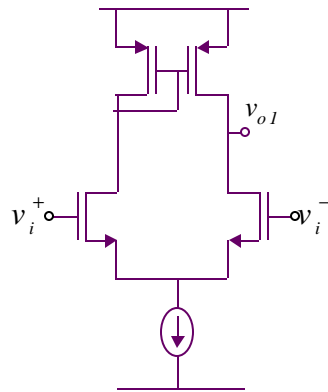
if the load resistance is much higher than  $R_{out}$



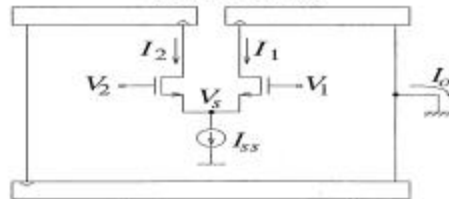
If the load is capacitor. ☺

i.e., Switched-Capacitor Circuits or  
open loop continuous-time  
Integrator

## Simple CMOS Operational Transconductor Amplifier (OTA)



### Basic OTA



$$\left. \begin{aligned} I_1 &= \beta (V_1 - V_s - V_T)^2 \\ I_2 &= \beta (V_2 - V_s - V_T)^2 \\ I_1 + I_2 &= I_{SS} \end{aligned} \right\} \Rightarrow V_s = \frac{V_1 + V_2 - 2V_T}{2} \pm \sqrt{\frac{I_{SS}}{2\beta} - \left(\frac{\Delta V}{2}\right)^2}$$

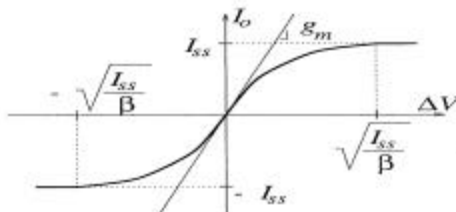
$$\Delta V = V_1 - V_2$$

$$I_o = I_1 - I_2 \Rightarrow I_o = \Delta V \sqrt{2I_{SS}\beta} \sqrt{1 - \frac{\beta}{2I_{SS}} (\Delta V)^2}$$

$$\beta = \frac{\mu C_{ox} W}{2L}$$

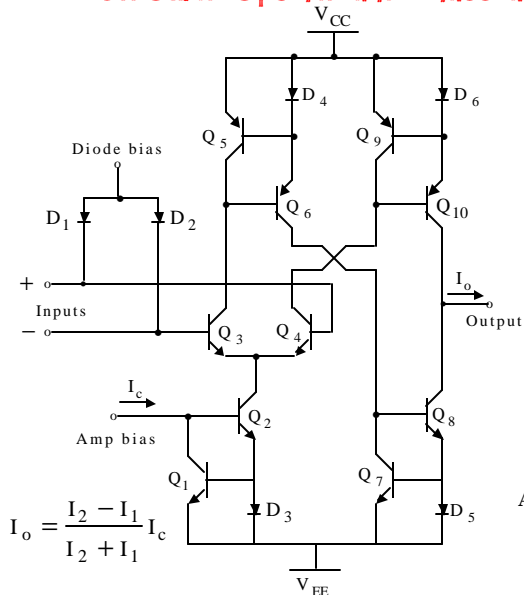
$$g_m = \sqrt{2I_{SS}\beta}$$

Linearity considerations

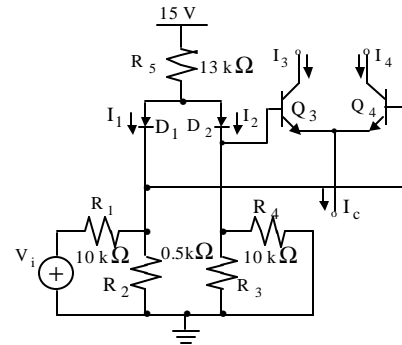




### BIPOLAR Operational Transconductor Amplifiers

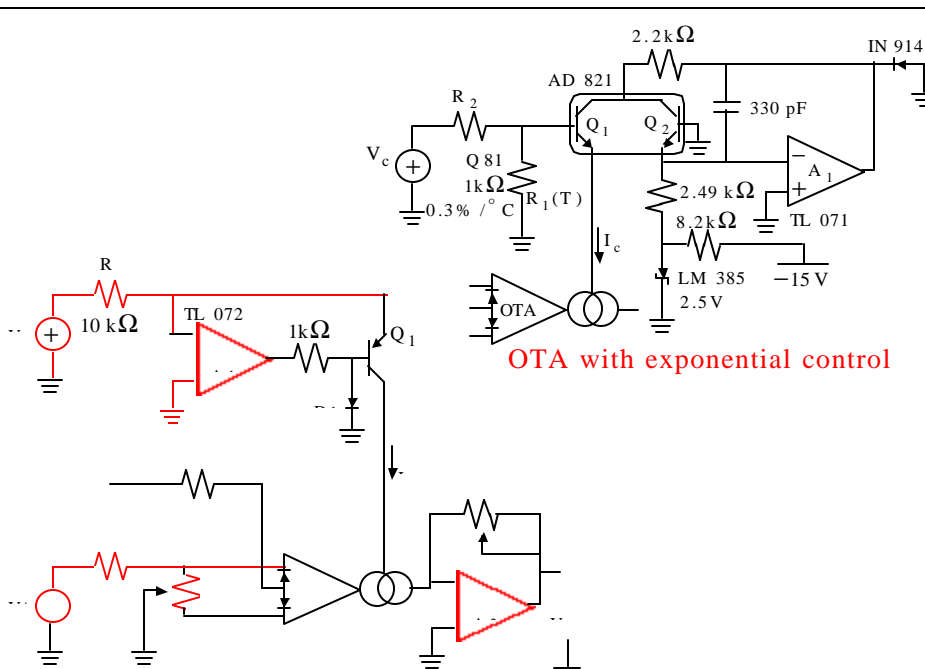


Bipolar OTA, LM13600 type.



An alternative linearization approach

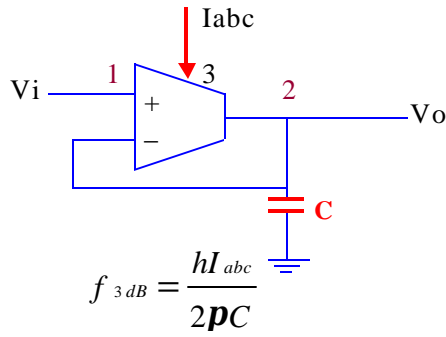
$$I_o = \frac{I_c}{12.2V} V_i$$



OTA with exponential control

Voltage-Controlled Amplifier with Linear Control.

### First-Order Low-Pass using one OTA and one capacitor



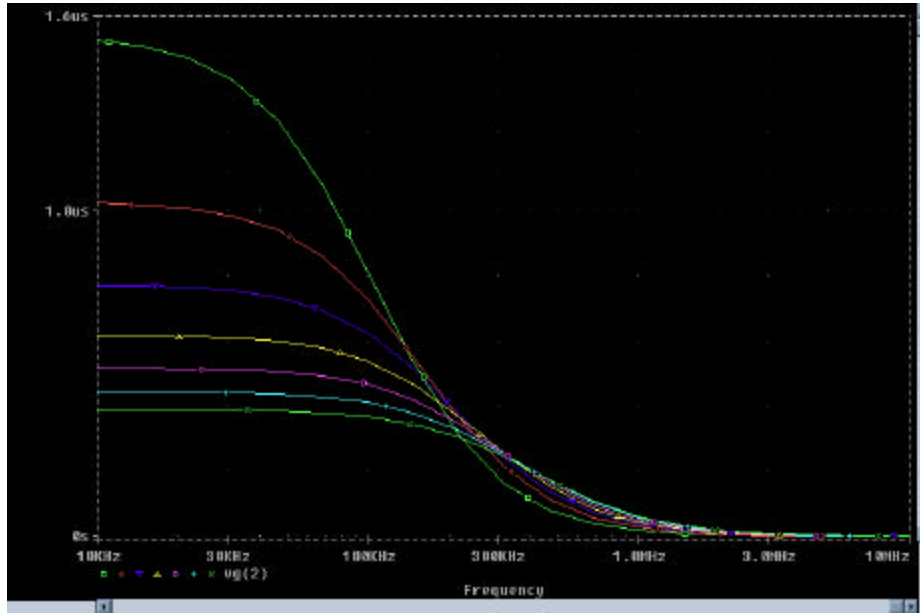
Vdd 7 0 15v  
Vss 8 0 -15V

100Khz <  $f_{3dB}$  < 400KHz

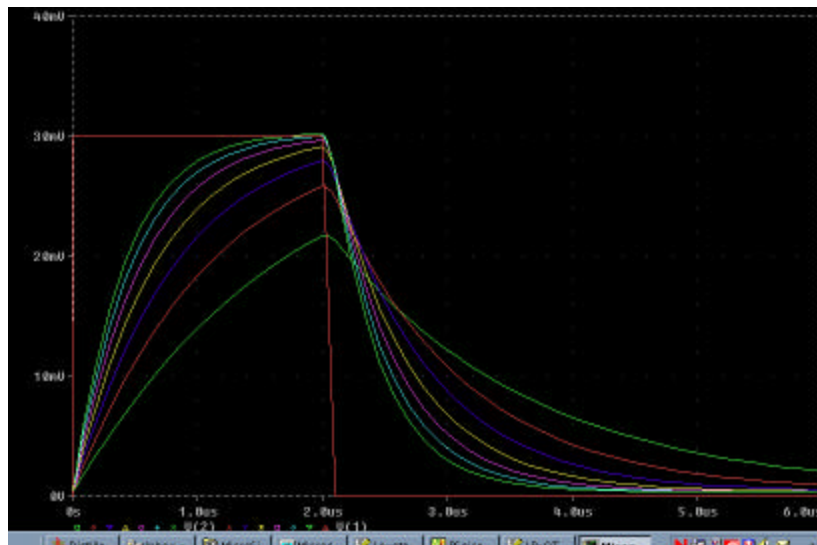
Note.- This OTA uses bipolar transistors



### Group Delay for a First-Order Programmable Low Pass



### Time Response (Pulse of 2µs duration) for a LP First-Order



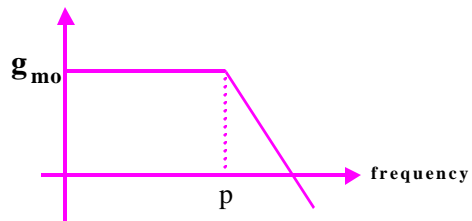
LM13600 with  $I_{bic} = \{0.1\text{mA}-0.4\text{mA}\}$

## OPERATIONAL TRANSCONDUCTANCE AMPLIFIER (OTA) Frequency Dependence

$$G_m = g_{mo} / (1 + s/p)$$

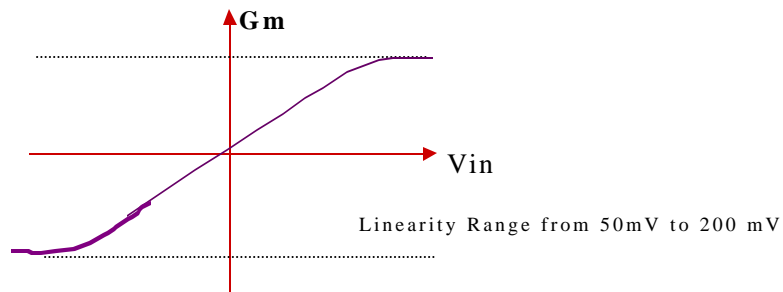
Where  $g_{mo}$  is the DC transconductance gain

$p$  is the dominant pole which is around 10MHz to 100Mhz

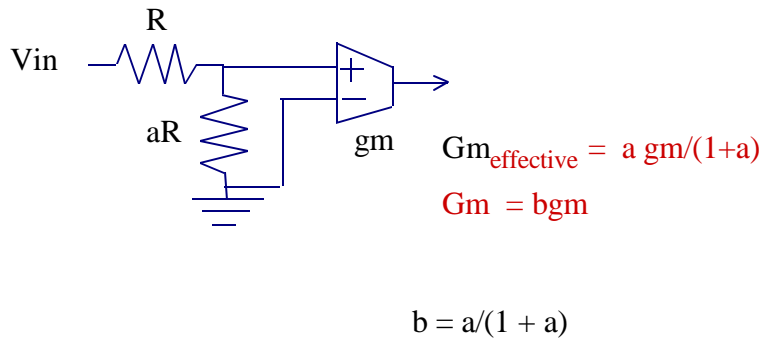


Issues about the OTA:

- Operated in open loop conditions
- High-Frequency Operation
- Poor Linearity Range

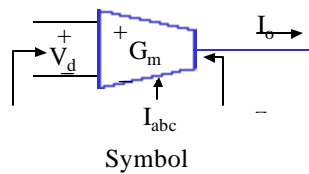


## Linearization of OTA by means of Attenuation



## Basic Building Blocks

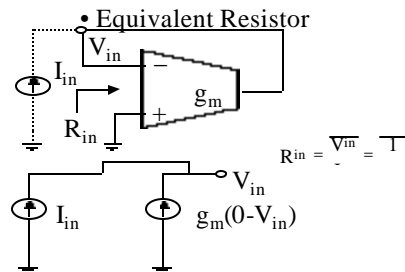
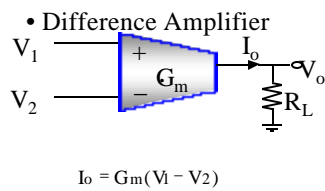
- The Operational Transconductor Amplifier (OTA)--its input is voltage; its output is current. It is a voltage-controlled current source.



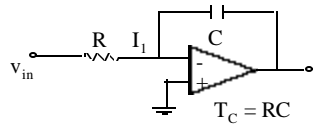
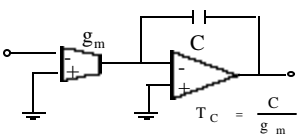
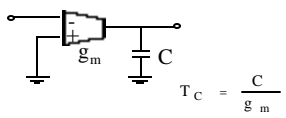
$$G_m = G_m(I_{abc})$$

### Fundamental Operations

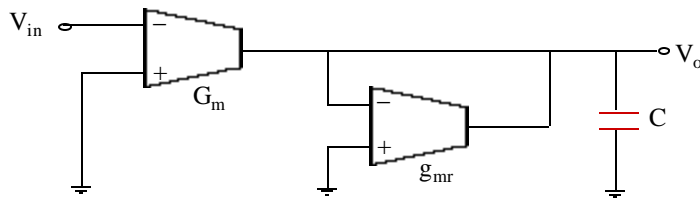
Observe that in contrast to Op Amp, the OTA is often used in an open-loop fashion.



## INTEGRATORS

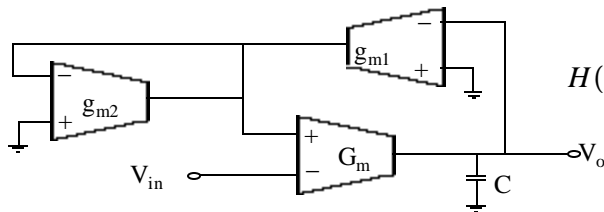
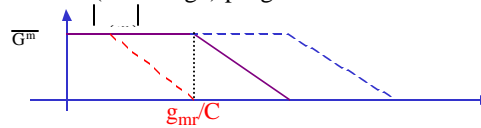
| Implementation  | Remarks  |
|---|--|
|  <p style="text-align: center;"><math>T_c = RC</math></p> <p>MOSFET-C, <math>T_c = \frac{C}{K(V_{c1} - V_{c2})}</math></p> | <ul style="list-style-type: none"> <li>• Non-ideal op amp effects i.e., <math>A_o</math>, GB</li> <li>• Frequency limitations <math>\omega_o = \frac{1}{T_c} &lt; GB</math>, i.e., <math>\omega_o \leq \frac{GB}{30}</math></li> <li>• Need of buffered op amp</li> <li>• Limited MOSFET's gate volt.</li> </ul> |
|  <p style="text-align: center;"><math>T_c = \frac{C}{g_m}</math></p>   | <ul style="list-style-type: none"> <li>• Increased tunability</li> <li>• No loading effect</li> <li>• Still GB effects</li> <li>• No parasitic cap. effects</li> </ul>   |
|  <p style="text-align: center;"><math>T_c = \frac{C}{g_m}</math></p>   | <ul style="list-style-type: none"> <li>• Need linear components</li> <li>• Excellent frequency resp.</li> <li>• MOSFET OTA tuning range of several octaves</li> <li>• BiCMOS OTA wider tuning range</li> <li>• Suffer parasitic cap. effects</li> </ul>  |

### • Low Pass (First-Order) Filter



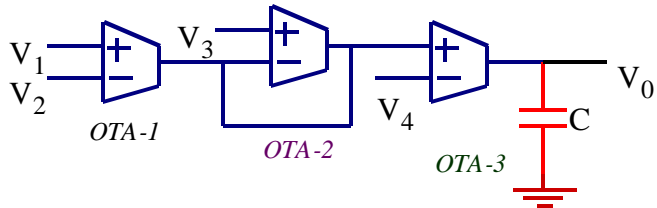
$$H(s) = \frac{V_o(s)}{V_{in}(s)} = \frac{-G_m}{sC + g_{mr}}$$

Remember that OTAs are current (or voltage) programmable.



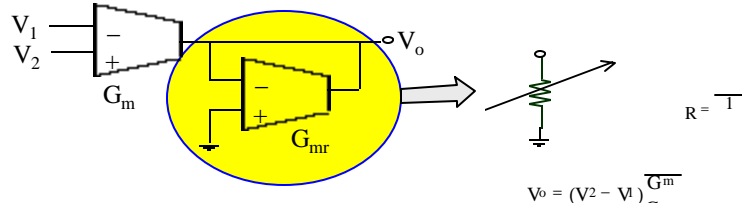
$$H(s) = \frac{V_o(s)}{V_{in}(s)} = \frac{-G_m}{sC + G_m g_{m1} / g_{m2}}$$

### Example of Multiple OTAs Circuit



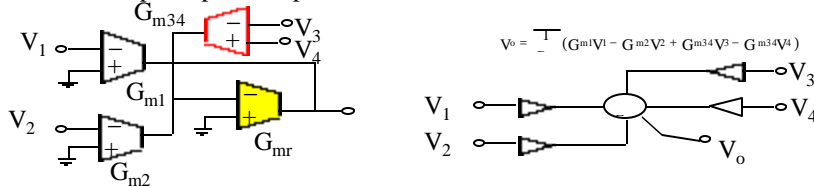
$$V_0 = \frac{1}{sC} (g_{m1}(V_1 - V_2)g_{m3} + (V_3 - V_4)g_{m3})$$

#### • Two OTAs Amplifier

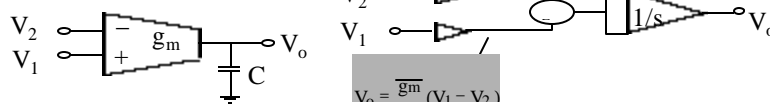


Observe that both inverting and non-inverting amplifiers are simultaneously available. If only one is needed, the other input is grounded.

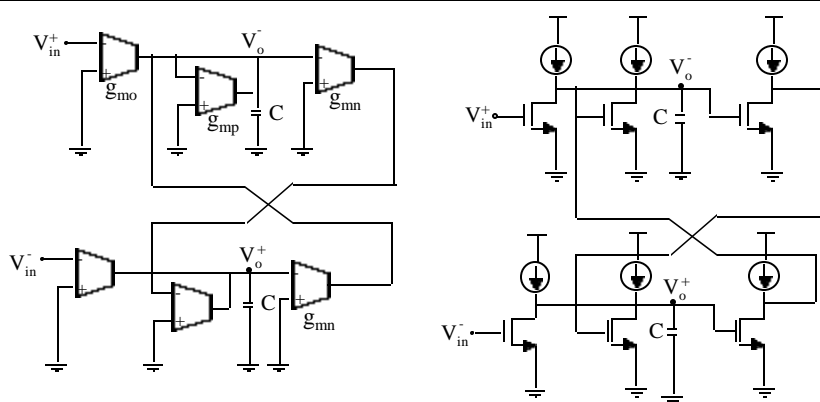
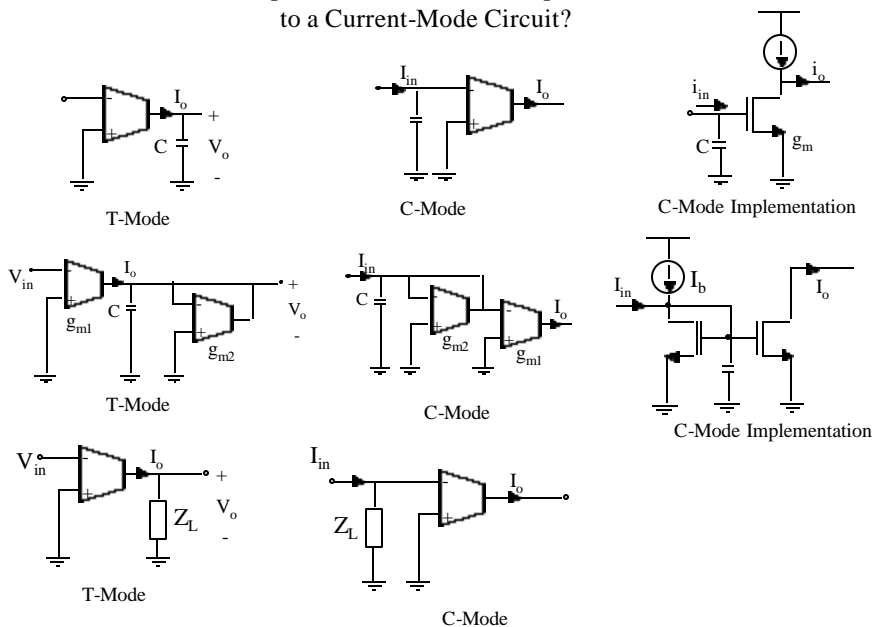
#### • Multiple Inputs Amplifier



#### • Integrator



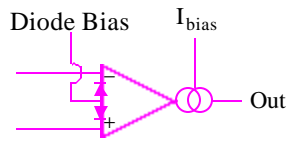
### How to map a Transconductance-Capacitor Circuit to a Current-Mode Circuit?



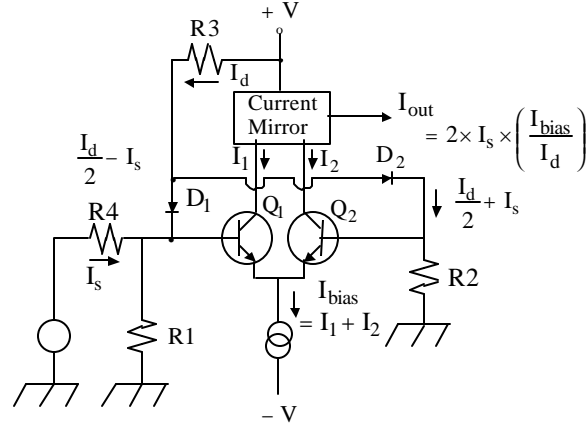
Pseudo-Differential Voltage-Mode Implemented with Transconductors

$$A_{dm} = \frac{g_{m0} / C}{S + (g_{mN} - g_{mP}) / C}$$

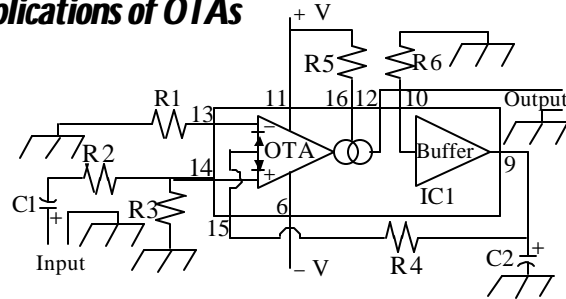
$$A_{cm} = \frac{g_{m0} / C}{S + (g_{mN} + g_{mP}) / C}$$



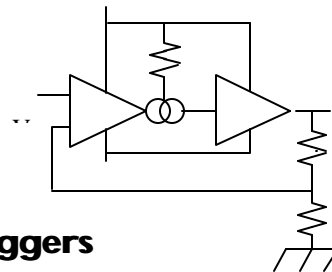
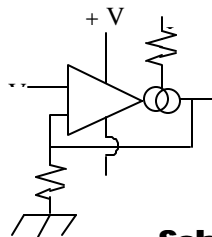
*LM 13600 simplified version*



**Applications of OTAs**



*Automatic Gain Control (AGC) Amplifier*



**Schmitt Triggers**

## REFERENCES

- [1] A. Rodríguez-Vázquez and E. Sánchez-Sinencio, editors, "Special Issue on Low Voltage and Low-Power Analog and Mixed-Signal Circuits and Systems," *IEEE Transactions on Circuits and Systems, Part I*, Vol. 42, November 1995.
- [2] B. Sheu, M. Ismail, E. Sánchez-Sinencio, and T. H. Wu, editors, *Micro-systems Technology for Multimedia Applications: An Introduction*, IEEE Press, New York 1995.
- [3] M. Ismail, T. Fiez, editors, "Analog VLSI Signal and Information Processing" McGraw Hill, Inc., New York 1994.
- [4] B. Bunch and A. Hellemans, editors, "The Timetables of Technology," A Touchstone Book, Simon & Schuster, New York 1994.
- [5] Y. P. Tsividis and J. O. Voorman, *Integrated Continuous Time Filters*, IEEE Press, New York 1993.

- [6] J. Ramírez-Angulo, M. Robinson, and E. Sánchez-Sinencio, "Current-Mode Continuous-Time Filters: Two Design Approaches," *IEEE Transactions on Circuits and Systems II*, Vol. 39, pp 337-341, June 1992.
- [7] R. Zele, S. S. Lee, G. Liang, and D. J. Allstot, "A Continuous-Time Current-Mode Integrator," *IEEE Transactions on Circuits and Systems*, Vol. 38, pp 1236-1238, October 1991.
- [8] J. B. Hughes, N. C. Bird and I. C. Macbeth, "Switched Currents A New Technique for Analog Sampled-Data Signal Processing," *Proc. IEEE/ISCAS*, pp 1584-1587, May 1989.
- [9] S. K. Mitra and C. F. Kurth, editors, "Miniaturized and Integrated Filters," John Wiley and Sons, New York 1989.
- [10] Y. Tsividis, M. Banu and J. Khoury, "Continuous-Time MOSFET-C Filters in VLSI," *IEEE Journal of Solid-State Circuits*, Vol. 21, pp 15-30, January 1986.
- [11] R. Gregorian and G. C. Temes, "Analog MOS Integrated Circuits for Signal Processing," Wiley Interscience, New York 1986

- [12] R. L. Geiger and E. Sánchez-Sinencio, "Active Filter Design Using Operational Transconductance Amplifiers: A Tutorial," *IEEE Circuits and Devices*, Vol. 1, pp 20-32, 1985.
- [13] P. E. Allen and E. Sánchez-Sinencio, "*Switched Capacitor Circuits*," Van Nostrand Reinhold, 1984.
- [14] A. S. Sedra and K. C. Smith, "*Microelectronic Circuits*," Holt, Rinehart and Winston, New York 1982.
- [15] P. R. Gray and R. G. Meyer, "*Analysis and Design of Analog Integrated Circuits*," First Edition John Wiley & Sons, New York 1977.
- [16] B. J. Hosticka, R. W. Brodersen, and P. R. Gary, "MOS Sampled-Data Recursive Filters using Switched-Capacitor Integrators," *IEEE Journal Solid-State Circuits*, Vol. SC-12, pp 600-608, December 1989.
- [17] J. T. Caves, M. A. Copeland, C. F. Rahim and S. D. Rosenbaum, "Sampled Analog Filtering using Switched Capacitors as Resistor Equivalents," *IEEE Journal Solid-State Circuits*, Vol. SC-12, pp 592-600, December 1977.